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Keywords: LED, boost, string, MAX16834, high voltage, step-up, driver

REFERENCE DESIGN 4612 INCLUDES: ✓Tested Circuit ✓Schematic ✓BOM ✓Board Available

Boost Driver for Long LED Strings Using Aluminum Electrolytic Capacitors

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Apr 29, 2010

Abstract: The long strings of LEDs commonly found in TV and display backlighting, street lights, and parking garage lights require a current driver capable of producing high voltages. This reference design provides such a driver using the MAX16834, and demonstrates how very-high dimming ratios can be obtained.

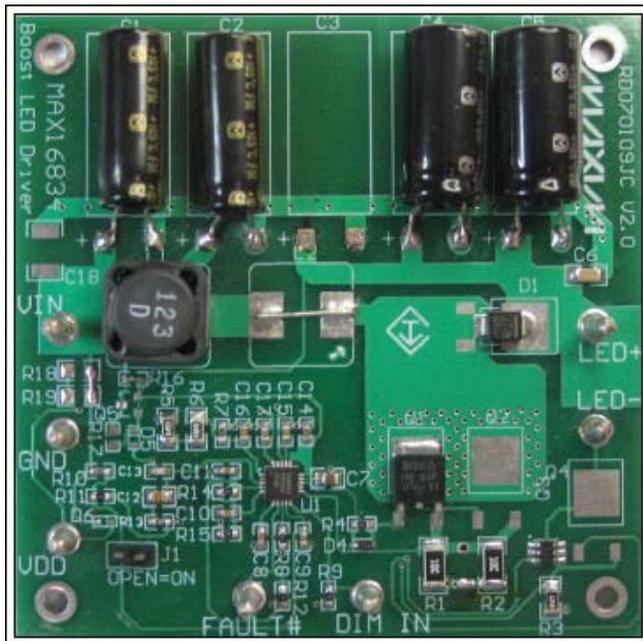
This is a reference design for a boost LED driver using the [MAX16834](#) for long strings of LEDs. This application is for LED backlighting for large LCD TVs or displays as well as streetlights and parking garage lights.

V_{IN} : 24VDC \pm 5% (at 1.22A)

V_{LED} Config.: 23 LEDs in series (75V) at 350mA.

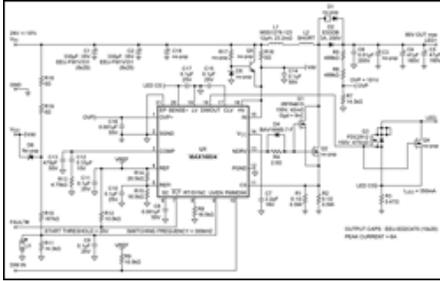
Dimming: As low as a 3.33 μ s on-pulse (3000:1 dimming ratio when the dimming frequency = 100Hz).

Note: this design has been built and tested. However, detailed testing has not occurred and there may be nuances that are yet to be discovered.

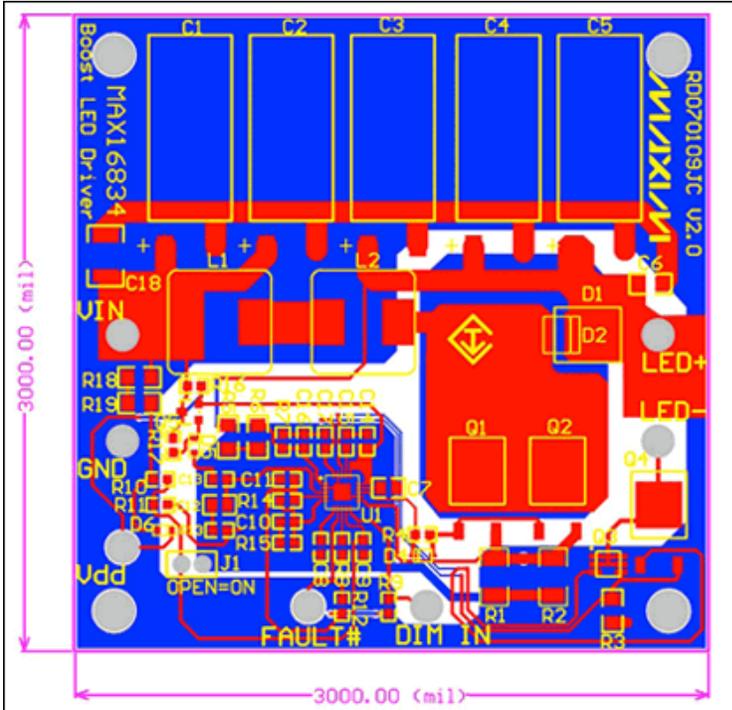


[More detailed image \(PDF, 3.53MB\)](#)

Figure 1. The LED driver board.



[More detailed image \(PDF, 295kB\)](#)
 Figure 2. Schematic of the LED driver.



[More detailed image \(PDF, 2.85MB\)](#)
 Figure 3. Layout of the LED driver.

Component list

Source Data From:

RD071408JC.PrjPCB

Project:

24VIN, 23LED, 350mA, MAX16834 Boost

Variant:

None

Creation Date:

Print Date:

#	Designator	LibRef	Comment	Footprint	Quant	Notes
1	C1, C2	CAPACITOR - POLARIZED	330uF,35V	CAPACITOR - 10X20	2	Panasonic-ECG
2	C3	CAPACITOR - POLARIZED	No-pop	CAPACITOR - 10X20	1	
3	C4, C5	CAPACITOR - POLARIZED	47uF,160V	CAPACITOR - 10X20	2	Panasonic-ECG
4	C6	CAPACITOR - NONPOLARIZED	0.01uF,200V,X7R	1206	1	Murata
5	C7	CAPACITOR - NONPOLARIZED	2.2uF,16V,X7R	0805	1	Murata
6	C8, C16	CAPACITOR - NONPOLARIZED	0.001uF,50V,X7R	0603	2	Murata
7	C9, C10, C11, C15, C17	CAPACITOR - NONPOLARIZED	0.1uF,25V,X7R	0603	5	Murata
8	C12	CAPACITOR - NONPOLARIZED	0.33uF,10V,X7R	0805	1	Murata
9	C13	CAPACITOR - NONPOLARIZED	470pF,50V,C0G	0603	1	Murata
10	C14	CAPACITOR - NONPOLARIZED	0.1uF,50V,X7R	0603	1	Murata
11	C18	CAPACITOR - NONPOLARIZED	No-pop	1812	1	
12	D1, Q2, Q4	DIODE - D2PAK, MOSFET - N	No-pop	TO-252 D-PAK	3	
13	D2	DIODE	ES3DB	SMB	1	Diodes, Inc
14	D4	DIODE	BAV16WS-7-F	SOD323	1	Diodes, Inc
15	D5, D6	DIODE - SCHOTTKY, DIODE - ZENER	no-pop	SOD-523	2	
16	L1	INDUCTOR	MSS1278-123	INDUCTOR - COILCRAFT MSS1278	1	Coilcraft
17	L2	INDUCTOR	SHORT		1	
18	Q1	MOSFET - N CHANNEL	IRFR4615	TO-252 D-PAK	1	International Rectifier
19	Q3	MOSFET - N TSSOP-6	FDC2512	SOT23-6	1	Fairchild
20	Q5	TRANSISTOR - NPN	no-pop	SOT23-3	1	
21	R1, R2	RESISTOR	0.1,0.5W	2010	2	
22	R3	RESISTOR	0.47	1206	1	
23	R4	RESISTOR	2.0	0603	1	
24	R5, R6	RESISTOR	499K	1206	2	
25	R7, R11	RESISTOR	14.3K	0603	2	
26	R8, R15	RESISTOR	16.5K	0603	2	
27	R9, R12	RESISTOR	10.0K	0603	2	
28	R10	RESISTOR	187K	0603	1	
29	R13	RESISTOR	4.75K	0603	1	
30	R14	RESISTOR	20.5K	0603	1	
31	R16	RESISTOR	0	0603	1	
32	R17	RESISTOR	no-pop	0603	1	
33	R18, R19	RESISTOR	0	1206	2	
34	U1	MAX16834	MAX16834	QFN-20 4X4	1	Maxim Integrated Products

[More detailed image \(PDF, 1.3MB\)](#)

Figure 4. Bill of materials.

Basic Discontinuous Boost Converter Design						Jim Christensen Maxim Integrated Products				
Spreadsheet is protected but can be changed to unprotected (no password)										
Legend:										
Input Values In Blue -- Adjust to match the circuit						Output Values In Yellow -- Read Only				
Inputs	Symbol	MIN	TYP	MAX	UNITS	Outputs	Symbol	MIN	MAX	UNITS
Input Voltage	V_{IN}	22.80		25.20	V					
Assumed Efficiency (except diode)	η		0.94							
Output LED Voltage	V_{LED}			80.00	V					
LED Current	I_{LED}			0.350	A					
Output Diode Voltage Drop	V_D	0.30		1.00	V					
Switching Frequency	f_{sw}		300.00		KHz					
Acceptable Output Voltage Ripple	$V_{ORIPPLE}$			0.18	V					
Current Sense Resistor	R_{CS}		0.05		Ω					
						Maximum Duty Cycle	DC_{MAX}		0.719	
						Maximum On Time	T_{ONMAX}		2.395	μsec
						Off Time	T_{OFFMAX}		3.333	μsec
						Output Power	P_{OUT}		28.000	W
						Maximum value of inductance	L_{MAX}	20.8		μH
Inductance Value Chosen	L	9.6	12	14.4	μH					
Series Resistance of L	R_L		0.14		Ω					
						L average current	I_{Lavg}		1.306	A
						L peak current	I_{Lpk}		4.012	A
						L RMS current	I_{Lrms}		1.869	A
						L Power Dissipation	P_L		0.489	W
						MOSFET RMS current	I_{MOSRMS}		1.649	A
						MOSFET peak current	I_{MOSpk}		4.012	A
						MOSFET peak voltage	V_{MOSpk}		81.000	V
						R_{CS} peak voltage	V_{RCSpk}		0.201	V
						Output capacitor RMS current	$I_{COUTRMS}$		0.905	A
						Output cap value (minimum)	C_{OUT}		5.704	μF

More detailed image (PDF, 900kB)

Figure 5. Design spreadsheet. To get the spreadsheet for use in your design, contact your local Maxim sales office.

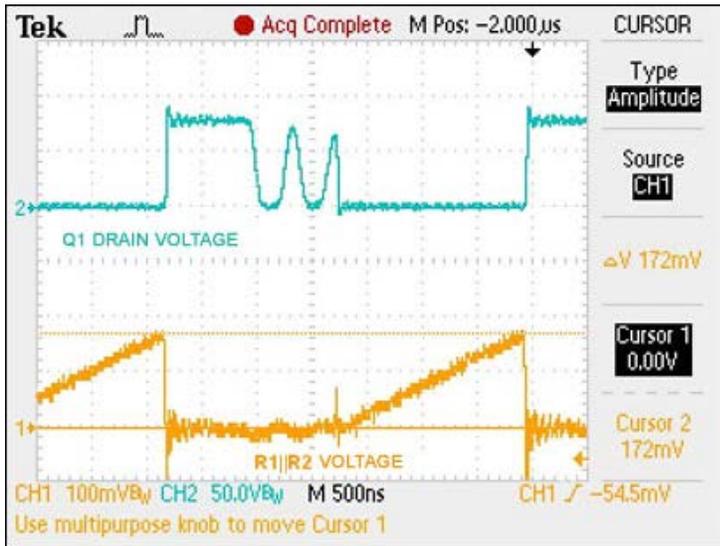


Figure 6. Drain voltage and current-sense resistor voltage (50m Ω).

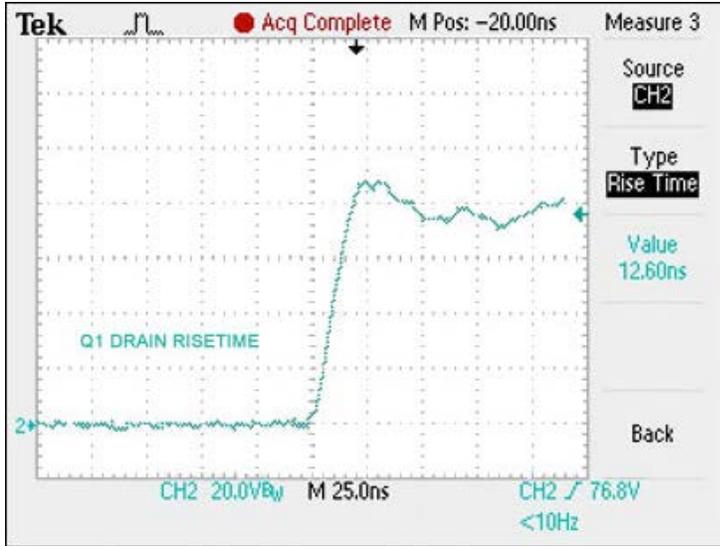


Figure 7. Drain voltage risetime.

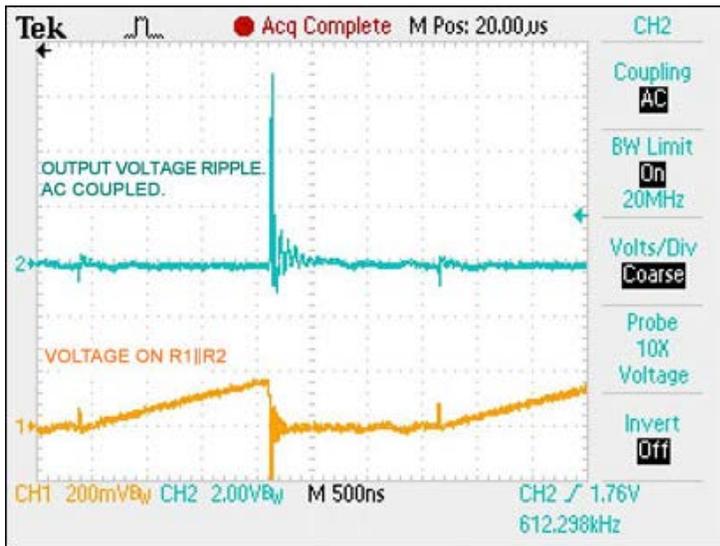


Figure 8. Output voltage (AC coupled) and sense-resistor voltage.

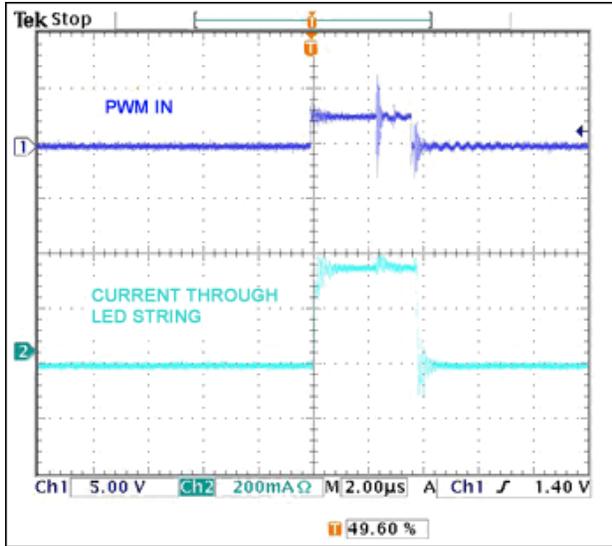


Figure 9. Figure 9. High dimming ratio (on-time < 4μs).

Inductor Core & Winding Loss Calculator

Step 1,2,3 Enter the operating conditions (all fields required)

Frequency	IL rms max	ΔIL peak-peak
<input type="text" value="300"/> kHz	<input type="text" value="1.90"/> Amps	<input type="text" value="4.01"/> Amps

Results (estimated)

	Inductor 1	Inductor 2	Inductor 3	Inductor 4
	MSS1278-123			
	<small>\$0.69 each at 1,000 qty.</small>			
Total inductor loss	<input type="text" value="575"/> mW	<input type="text"/> mW	<input type="text"/> mW	<input type="text"/> mW
Inductor core loss	<input type="text" value="452"/> mW	<input type="text"/> mW	<input type="text"/> mW	<input type="text"/> mW
DCR loss	<input type="text" value="116"/> mW	<input type="text"/> mW	<input type="text"/> mW	<input type="text"/> mW
AC winding loss	<input type="text" value="8"/> mW	<input type="text"/> mW	<input type="text"/> mW	<input type="text"/> mW
Temperature rise	<input type="text" value="27"/> °C	<input type="text"/> °C	<input type="text"/> °C	<input type="text"/> °C

This loss calculator is intended to provide the best possible estimate of inductor losses over a range of frequencies, load currents and ripple currents. Actual performance may vary based on operating conditions and should always be verified experimentally for each application.

Figure 10. Inductor temperature rise. The calculator is available from Coilcraft®.

Circuit Description

Overview

This reference design is for a high-voltage, boost current source for very long strings of LEDs. Applications include LCD TV backlighting, LCD monitor backlighting, streetlights, and parking garage lights. Long LED strings can be a very cost-effective way to drive LEDs. Also, since the LEDs will have exactly the same current, brightness variations are nicely controlled. This design has a 24V input, up to an 80V LED output, and drives 350mA through the LED string.

The measured input power is 29.3W and the output power is 26.4W for about 90% efficiency.

PCB

The printed circuit board (PCB) is a general-purpose board for MAX16834 boost designs (**Figures 1 and 3**). Therefore, **there are many components that are either shorted or not populated**. These components are indicated on the schematic (**Figure 2**). **Figure 4** shows a bill of materials for this design.

Topology

This design is for a 300kHz discontinuous-boost regulator. In **Figure 5**, the spreadsheet printout shows the calculated RMS and peak currents in the MOSFET and inductor. Discontinuous designs **do, admittedly, have some disadvantages, notably higher MOSFET and inductor currents**. However, since the output current is essentially zero when the MOSFET (Q1) turns on, the reverse recovery losses in the output diode (D2) are minimal. **This advantage outweighs the design disadvantages, because overheating and noise caused by reverse-recovery currents are difficult to manage**. Inspecting the circuit waveforms in **Figure 6**, you see that the on-time of the MOSFET is about 1.6 μ s. Once the MOSFET turns off, the drain voltage jumps to 75V for about 1 μ s, while the inductor conducts to the output capacitors. After that, the inductor energy is essentially drained, and for another microsecond the inductance and MOSFET output capacitance ring until the next on-time.

MOSFET Drive

Because of the discontinuous design, the peak MOSFET currents are more than twice what they would be with a continuous design. However, since there is no current through the MOSFET during turn-on, it only experiences switching losses during turn-off. The MAX16834 drives the MOSFET hard enough for the switch to turn off in about 20ns (**Figure 7**), thereby keeping the temperature rise low. If EMI becomes a problem, the series resistance and diode on the MOSFET gate can be altered to adjust the switching times. If needed, place a second MOSFET, Q2, parallel to Q1 to reduce the temperature rise.

Output Capacitance

For the input and output capacitance, the driver uses long-life electrolytic capacitors. Electrolytic capacitors are neither as durable nor as small as ceramic capacitors, but they have the advantage of providing plenty of capacitance at an economical price. To maintain a low profile (10mm), the capacitors lie in a horizontal orientation. The input and output capacitors are rated for 4000 hours and 8000 hours, respectively, at a temperature of +105°C. As a general rule, electrolytic capacitors double their lifetimes for every 10°C reduction of ambient temperature. This means that for an ambient of +65°C, you can expect the input/output capacitors to maintain performance for 64kHrs/128kHrs. In **Figure 5** the spreadsheet printout indicates that, to achieve the desired output-ripple voltage, you need only about 6 μ F of output capacitance. Because electrolytic capacitors have a limited ripple-current capability, this design uses two 47 μ F capacitors. The large amount of capacitance eliminates most of the switching-frequency ripple voltage (**Figure 8**). However since the capacitance is electrolytic with significant equivalent series inductance (ESL), the circuit noise created when the switching MOSFET turns off is not fully filtered. Adding ceramic capacitance or a low-Q LC filter on the output reduces this problem. Since each of these options has some cost, it is best to determine whether there is a problem with the high-frequency spike before trying to fix it.

Dimming

The MAX16834 is well suited for dimming. When PWMDIM (pin 10 of the IC) goes low, three things happen. First, the gate drive (pin 13) of the switching MOSFET, Q1, goes low. This prevents additional energy from being delivered to the LED string. Second, the gate drive (pin 18) of the dimming MOSFET, Q3, goes low. In addition to immediately curtailing the LED string current, the dimming MOSFET holds the voltage on the output capacitors constant during the off-time. Finally, to keep the compensation capacitance frozen at a steady-state voltage, the COMP (pin 3) goes to high impedance. The high impedance of the COMP pin ensures that the IC will start at the correct duty cycle immediately after PWMDIM returns high. Each of these actions, plus the fact that in a discontinuous design the inductor starts at zero current for every cycle, allows for very short PWM on-times, and thus, high dimming ratios. The only practical limitation to the dimming ratio is the frequency of the main switching driver. Since this design is for 300kHz, the smallest PWM on-time is about 3.33 μ s, which implies a dimming ratio up to 1500:1 (at a 200Hz dimming frequency). **Figure 9** shows the current through the LED string with an on-time of less than 4 μ s. The LED string current is well behaved and provides the full 350mA during the pulse.

OVP

If the LED string were to open, the overvoltage protection (OVP) circuitry of the MAX16834 shuts down the driver for about 400ms between retry attempts. This design sets the OVP trip threshold to 101V.

FAULT#

The MAX16834 provides an output signal called FAULT#. This signal goes low whenever any internal fault (overcurrent or overvoltage) is detected. Once the fault is removed, FAULT# returns high. FAULT# is not latching.

Temperature Rise

Due to the high efficiency of the circuit (~90%), the components of the driver remain cool. The obvious exception is the inductor, which has a +49°C rise that is higher than the Coilcraft predictor in **Figure 10** (+27°C rise). The predictor loses accuracy when the peak currents exceed twice the RMS currents, which happens in discontinuous designs. For applications with high ambient temperatures, it may be necessary to use an automotive-rated inductor (+125°C) or use two 6µH inductors in series. For many applications with lower ambient temperatures, the single 12µH inductor would be acceptable.

Temperature Measurements

The following temperatures were measured using actual LED loads:

V _{IN} :	24VDC	
Ambient:	+22°C	ΔT
L ₁ :	+71°C	49°C
D ₂ :	+43°C	21°C
Q ₂ :	+38°C	16°C
Q ₃ :	+34°C	12°C

Power-Up Procedure

1. Attach a string of up to 23 LEDs between the LED+ post and LED- post.
2. Attach a 24V, 2A power supply between the V_{IN} post and GND post.
3. If dimming is desired, attach a PWM signal (0 to 5V) to the DIM IN post and GND post.
4. Turn on the 24V power supply.
5. Adjust the PWM duty cycle, as desired, to obtain dimming.

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Related Parts

[MAX16834](#)

High-Power LED Driver with Integrated High-Side LED Current Sense and PWM Dimming MOSFET Driver

[Free Samples](#)

More Information

For Technical Support: <http://www.maximintegrated.com/support>

For Samples: <http://www.maximintegrated.com/samples>

Other Questions and Comments: <http://www.maximintegrated.com/contact>

Application Note 4612: <http://www.maximintegrated.com/an4612>

REFERENCE DESIGN 4612, AN4612, AN 4612, APP4612, Appnote4612, Appnote 4612

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