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APPLICATION NOTE 4050

Current Sensing on a Negative Voltage Supply Rail, using a Precision Instrumentation Amplifier

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Abstract: Applications like ISDN and telecom systems need a negative voltage, current-sense amplifier. This application note describes one method for designing a negative-rail, current-sense amplifier. The design is quite flexible and can be easily changed for monitoring different negative rails. The MAX4460 single-supply instrumentation amplifier is used to demonstrate the design.

Introduction

High-side current-sense amplifiers are used principally for monitoring the current from a positive supply rail. Applications like ISDN and telecom power supplies, however, require current-sense amplifiers that operate at negative rail. This application note describes one method for designing a negative-rail, current-sense amplifier.

Application Example

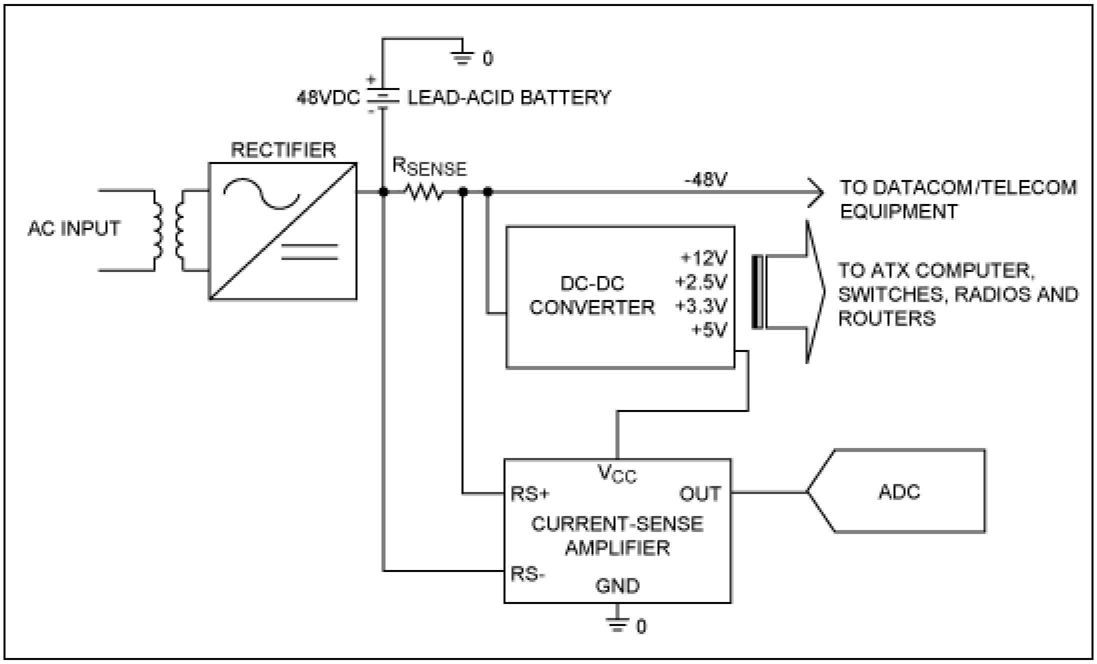

Figure 1. Block diagram of a telephone central-exchange, power-supply system.

Figure 1 shows a block diagram of the power-distribution network in a typical telephone exchange. A rectifier converts the AC at the power mains to DC, and the DC output from the rectifier is used to charge a 48V lead-acid battery. The battery powers the user telephones through the telephone line. The battery polarities are connected so that the line voltage is negative (-48V). A negative line voltage helps to reduce the corrosion from electrochemical reactions occurring on a wet telephone line. A telecom network also uses several DC-DC converters to derive intermediate power-supply rails from the -48V DC input. The intermediate power supply rails power the switches, radios, routers, ATX computers, and other electronic equipment in the telephone exchange. A current-sense amplifier oversees the system health by monitoring the -48V power-supply current.

Circuit Description

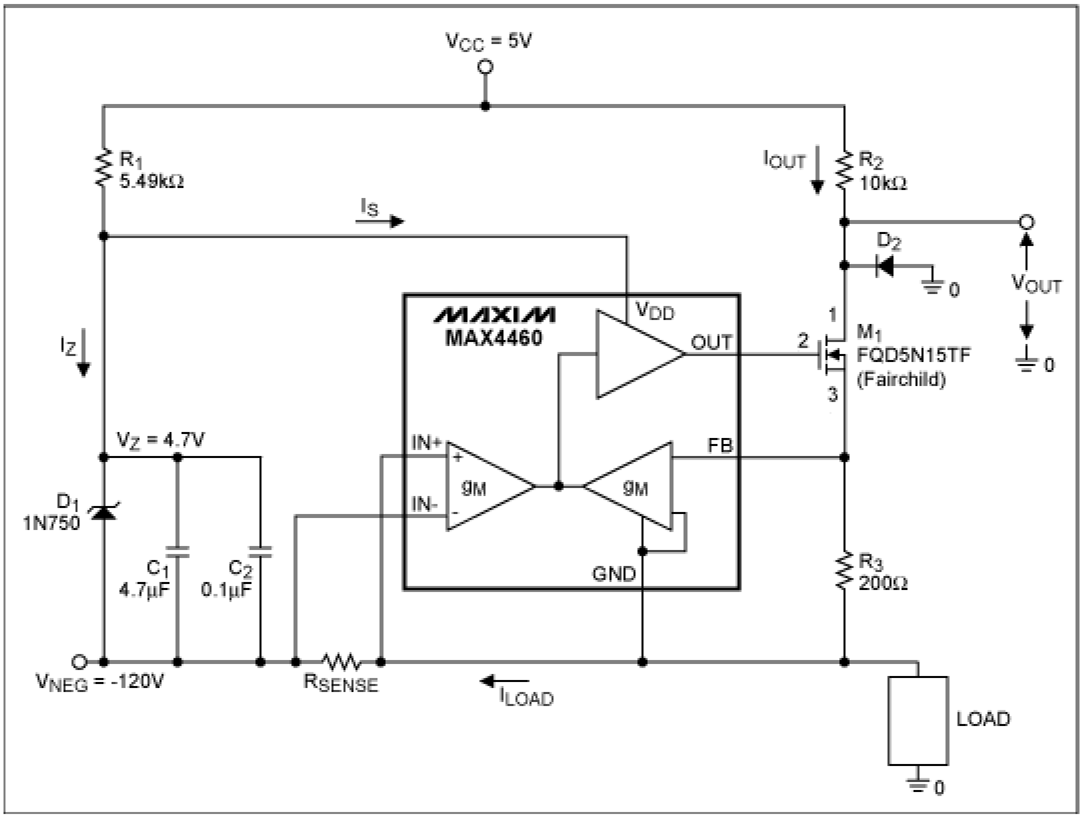

Figure 2. Negative-rail, current-sense amplifier using the MAX4460.

The circuit in **Figure 2** shows an implementation of the negative-rail, current-sensing block. It uses an instrumentation amplifier like the MAX4460 or the MAX4208 and some discrete components.

The zener diode, D_1, protects the instrumentation amplifier from overvoltage damage while providing sufficient supply voltage for its operation. The current to be monitored flows to the negative supply through the sense resistor, R_{SENSE}. The instrumentation amplifier must have a single supply and operate with a ground-sensing capability.

The MAX4460's output provides the gate drive for MOSFET M_1. Negative feedback ensures that the voltage drop across resistor R_3 equals V_{SENSE}, the voltage across R_{SENSE}. Consequently, R_3 sets a current proportional to the load current:

$$I_{OUT} = (I_{LOAD} \times R_{SENSE})/R_3 = V_{SENSE}/R_3 \qquad \text{(Eq. 1)}$$

R_2 is chosen so that the output voltage lies within the desired range of the following circuit, typically an ADC. The drain-source breakdown voltage rating of the MOSFET must exceed the total voltage drop between the two supply rails (+125V in this case). An additional op-amp buffer can be used at V_{OUT} if the ADC does not have a high-impedance input. If the sense current increases above the rated value during a fault condition, then the output voltage goes negative. Diode D_2 protects the ADC from damage by limiting the negative voltage at output to one diode drop.

Design Steps

The above design can easily be adapted to add high-voltage, negative supply, current-sense monitoring capability. This flexibility is illustrated by choosing -120V as the negative rail. By using the following straightforward steps, one can design a current-sense amplifier for a different supply rail.

1. Specify the Zener Regulator

It is important to bias the zener on a point in its transfer characteristic that gives a low dynamic resistance (i.e., well into its reverse breakdown region) to prevent PSRR errors. **Figure 3** shows a plot of the zener current versus the zener voltage for a standard zener diode configured in reverse bias. Data show that the zener voltage is not well-regulated close to the breakdown voltage. A general rule then is to select the bias point to be about 25% of the maximum current specified by the power rating. This bias point gives a low dynamic resistance without wasting too much power. The bias point is set to the desired value by choosing the resistor, R1, based on the following equation:

$I_{R1} = (V_{CC} + |V_{NEG}| - V_Z)/R_1 = I_S + I_Z$ (Eq. 2)

Where:
V_{CC} = Positive rail-supply voltage
V_Z = Regulated zener voltage
$|V_{NEG}|$ = Absolute value of the negative-rail voltage
I_S = Supply current for MAX4460
I_Z = Current through the zener diode

R_1 must have a suitable power rating and be able to withstand the large voltages across it. Alternatively, one can use a series-parallel combination of lower wattage resistors to ease these constraints.

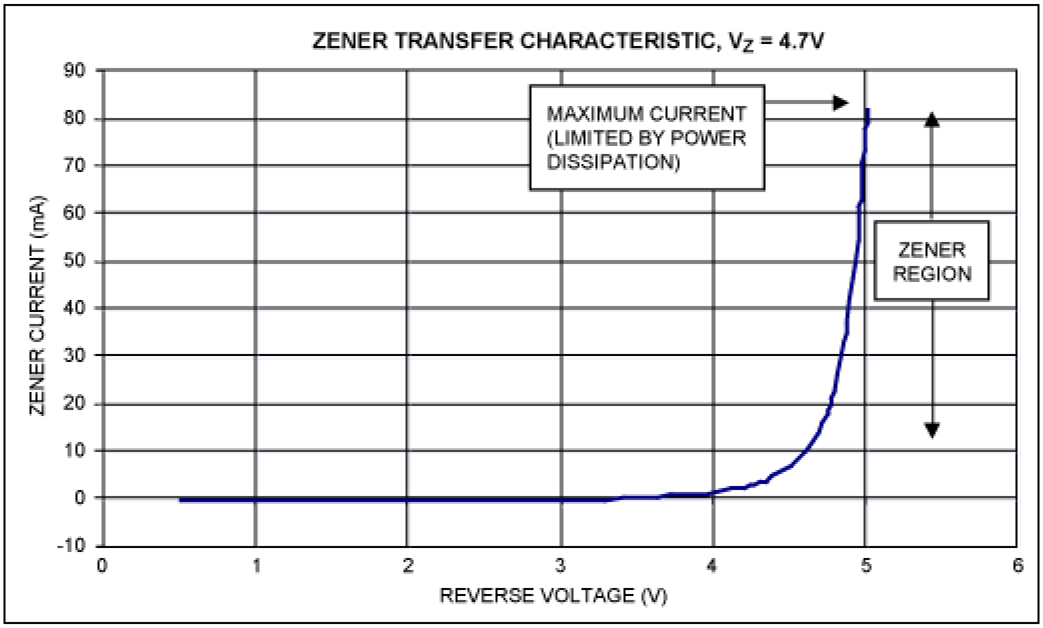

Figure 3. 1N750 Zener diode transfer characteristic, V_Z = 4.7V.

2. Select the Power Transistor

The n-channel MOSFET, or JFET, must have a drain to source breakdown voltage rating greater than $|V_{NEG}| + V_{CC}$. This is an important constraint if the negative supply voltage is high.

3. Choose R_{SENSE}

Select R_{SENSE} so that the full-scale, sense voltage across R_{SENSE} is less than or equal to 100mV.

4a. Select R_3

There is considerable flexibility in choosing R_3. A good selection is influenced by the following two observations:

1. As R_3 is reduced, Equation 1 implies that for a fixed gain, the dissipated power increases.
2. The thermal noise and leakage current of the FET set the upper limit on the selected value of R_3.

4b. Select R_2

The ratio of resistors R_2 and R_3 equals the voltage gain of the resulting current-sense amplifier. The output voltage is given as:

$V_{OUT} = V_{CC} - I_{OUT} \times R_2$ (Eq. 3)

From Equations 1 and 3 we get:

$V_{OUT} = V_{CC} - (V_{SENSE} \times R_2/R_3)$

Differentiating with respect to V_{SENSE}:

Voltage gain, $A_v = -R_2/R_3$ (Eq. 4)

The negative sign represents the inverting relationship between the output voltage and the input sense voltage. From Equation 4, R_2 can thus be determined.

Results

Figure 4 plots the resulting typical output voltage as a function of the sense voltage. The following typical parameters can be inferred for the current-sense amplifier:

Input referred offset voltage = (5 - 4.9831)/49.942
= 338µV

Gain = -49.942

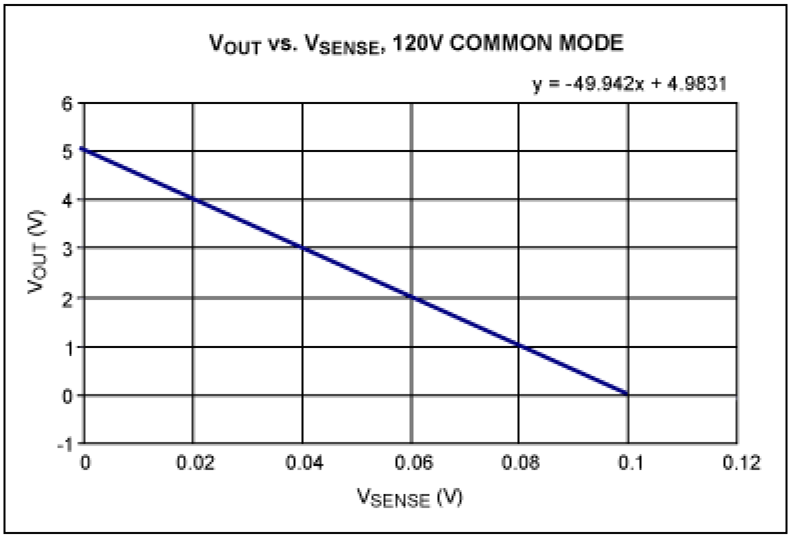

Figure 4. Output voltage variation with variation in sense voltage at T = +25°C.

Conclusion

This application note demonstrates the use of a precision, instrumentation amplifier like the MAX4460 for current sensing of a negative voltage. The described circuit can be easily redesigned for monitoring different negative rails by following the design steps listed above.

A similar article appeared in the August, 2007 issue of *Power Electronics Technology* magazine, a Penton Publication.

Related Parts		
MAX4208	Ultra-Low Offset/Drift, Precision Instrumentation Amplifiers with REF Buffer	Free Samples
MAX4460	SOT23, 3V/5V, Single-Supply, Rail-to-Rail Instrumentation Amplifiers	Free Samples
MAX9918	-20V to +75V Input Range, Precision Uni-/Bidirectional, Current-Sense Amplifiers	Free Samples
MAX9919	-20V to +75V Input Range, Precision Uni-/Bidirectional, Current-Sense Amplifiers	Free Samples
MAX9920	-20V to +75V Input Range, Precision Uni-/Bidirectional, Current-Sense Amplifiers	Free Samples
MAX9928F	-0.1V to +28V Input Range, Micropower, Uni-/Bidirectional, Current-Sense Amplifiers	Free Samples
MAX9929F	-0.1V to +28V Input Range, Micropower, Uni-/Bidirectional, Current-Sense Amplifiers	Free Samples

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